Final Exam: CE132
Tuesday May 12

## 8:10am-11am

| Problem | Score |
| :--- | ---: |
| $\# 0$ | $\{0,-2\}$ |
| $\# 1$ | $/ 25$ |
| $\# 2$ | $/ 25$ |
| $\# 3$ | $/ 15$ |
| $\# 4$ | $/ 15$ |
| $\# 5$ | $/ 10$ |
| $\# 6$ | $/ 10$ |
| Total | $/ 100$ |

Name

## SID

Permitted Materials: Open book, open notes, open Matlab and Mathematica.
Prohibited: Use of the internet and any and all communication devices (except to access bCourses and gradescope)

Honor Code: I have not given or received aid in this examination. I have taken an active part in seeing to it that others as well as myself uphold the spirit and letter of this Honor Code.

## (Signature)

No questions permitted during exam. If you have a concern about the wording of a question, explain your concern along with your answer.
0. ( 0 pts ) Copy the honor code at the top of your first answer page and sign your name to it, failure to do both ( -2 pts ).

1. (25 pts) An $L=5 \mathrm{~m}$ long beam with Young's modulus $E=200 \mathrm{GPa}$ has been loaded at its ends with possibly moments and shear forces.


The curvatures of the beam $\kappa_{x}$ and $\kappa_{y}$ have been measured as a function of $z$ to be constants:

$$
\begin{align*}
& \kappa_{x}=0.001 \mathrm{~m}^{-1}  \tag{1}\\
& \kappa_{y}=0.003 \mathrm{~m}^{-1} \tag{2}
\end{align*}
$$

The beam has the following moments of inertia

$$
\begin{equation*}
I_{x}=8.0 \times 10^{-3} \mathrm{~m}^{4} \quad I_{y}=5.0 \times 10^{-3} \mathrm{~m}^{4} \quad I_{x y}=3.0 \times 10^{-3} \mathrm{~m}^{4} \tag{3}
\end{equation*}
$$

Determine the end moments and shear forces that have been applied to the beam.
2. (25 pts) Shown is the cross-section of a thin-walled torsional member. The outer walls have thickness $t$ and the inner wall has a thickness of $t / 4$.


Assume $t=1 \mathrm{~mm}, a=300 \mathrm{~mm}, b=400 \mathrm{~mm}$, and $G=100 \mathrm{kN} / \mathrm{mm}^{2}$.
(a) Find the effective torsional stiffness of the structural member; i.e., find $T / \bar{\theta}=$ $(G J)_{\text {eff }}$.
(b) Find the max shear stress and the location where it occurs.
3. (15 pts) Consider a pin-pin column subjected to an axial load $P$ of length $L$ and radius of gyration $r$. Assume the column is made of an elastic-plastic material with the following stress-strain relation

$$
\sigma=\left\{\begin{array}{lr}
E \epsilon & \epsilon<\epsilon_{Y}  \tag{4}\\
\left(Y_{\infty}-Y_{o}\right)\left(1-e^{-\left(\epsilon-\epsilon_{Y}\right)}\right)+Y_{o} & \epsilon>\epsilon_{Y}
\end{array}\right.
$$

where $E$ is the Young's modulus, $Y_{o}$ is the initial yield stress, $Y_{\infty}$ is the yield stress at large strain, and $\epsilon_{Y}$ is the initial yield strain.



Assume that the column slenderness $L / r$ is such that the critical buckling stress

$$
\begin{equation*}
\sigma_{\mathrm{cr}}>Y_{o} \equiv E \epsilon_{Y} \tag{5}
\end{equation*}
$$

Determine the (critical) buckling stress for the column in terms of the material parameters and the slenderness ratio, $L / r$.
4. (15 pts) Consider an axisymmetric conical hopper which is supported by a ring support at half-height. The shell wall is uniform of thickness $t$.


The hopper is filled with a granular material that generates normal and tangential wall pressures

$$
\begin{align*}
p_{n}(z) & =-k\left(1-e^{-z / \zeta}\right)  \tag{6}\\
p_{t}(z) & =k\left(1-e^{-z / \zeta}\right) \tag{7}
\end{align*}
$$

where $k$ and $\zeta$ are given constants.
Find the hoop and meridional membrane resultants, $N_{\theta}(z)$ and $N_{\varphi}(z)$.
Express your answer in terms of $k, \zeta, z, H$, and $\alpha$.
Useful facts:
(a) $\varphi=\frac{\pi}{2}+\alpha$;
(b) $\sin (\varphi)=\cos (\alpha)$;
(c) $\cos (\varphi)=-\sin (\alpha)$.
5. (10pts) An open-ended thick-walled cylinder of inner radius $a=40 \mathrm{~mm}$ and outer radius $b=60 \mathrm{~mm}$ is subjected to a time varying internal sawtooth pressure $p_{i}(t)$ with maximum pressure $p_{\text {max }}$.


The cylinder also has a detected crack-like flaw of size $a_{i}=1 \mathrm{~mm}$ oriented orthogonal to the hoop direction. Determine
(a) the magnitude of $p_{\max }$ such that the cylinder will not fail before $N=10^{6}$ pressurization/depressuriztion cycles;
(b) the critical crack size for the pressure that you computed in part (a).

Assume
(i) the configuration correction factor for the crack is $Q=1.8$, i.e., $K_{\mathrm{I}}=Q \sigma_{\text {hoop }} \sqrt{\pi a}$;
(ii) the Young's modulus $E=200 \mathrm{kN} / \mathrm{mm}^{2}$;
(iii) the critical stress intensity factor is $K_{\mathrm{Ic}}=10 \mathrm{MPa} \sqrt{\mathrm{m}}$;
(iv) the Paris crack growth exponent $m=4$;
(v) the Paris crack growth coefficient $C=5.0 \times 10^{-13}(\mathrm{~m} / \mathrm{cycle}) /(\mathrm{MPa} \sqrt{\mathrm{m}})^{4}$.
6. (10 pts) Consider a clamped circular plate of radius $R$ with plate modulus $D$, both given. The plate is subjected to a pressure

$$
\begin{equation*}
p(r)=p_{o}\left(1-\frac{r}{R}\right) \tag{8}
\end{equation*}
$$

where $p_{o}$ is a given constant.
(a) Determine the expression $w(r)$ for the deflection of the plate, specialized for the given pressure loading; write your answer in a format that still includes the 4 (four) integration constants.
(b) State why you may a priori assume one of the integration constants to be zero.
(c) State the 3 (three) boundary conditions that you would use to solve for the remaining integration constants. Be reasonably specific but there is no need to actually solve for the constants - its just messy algebra.

